

Appendix D

Structural Hand Calculations for Slab Redesign



1430 Spring Hill Road, Suite 450
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 (703) 442-6500
 Fax (703) 442-8010

NOTES

TO _____
 FROM _____
 DATE _____ TIME _____
 PROJECT _____
 PROJECT NUMBER _____

MEMO CONFERENCE TELECON

ATTENDEES:

14' x 18' PANEL $\rightarrow l_2/l_1 = 1.29$

$f'_c = 4,000$ psi $f_y = 60,000$ psi

8" DROP PANELS

LIVE LOAD = 30 psf SNOW: 30 psf GREEN ROOF: 26 psf SELF: 100 psf

$h = 8" > 4"$ NO BEAMS $\therefore \alpha = 0$ & $\beta_e = 0$

$w_u = 1.2D + 1.6L_r + 0.5S$

$w_u = 1.2(26 + 100) + 1.6(30) + 0.5(30) = 214$ psf

STRIP SPAN

$$M_o = \frac{w_u l_n^2}{8} = \frac{(0.214)(18)(12.83)^2}{8} = 79.3 \text{ ft-k}$$

FROM ACI 13.6.3:

INT. NEG. $M_u = 0.70 M_o = 55.5 \text{ ft-k}$

EXT. NEG. $M_u = 0.26 M_o = 20.6 \text{ ft-k}$

POS. $M_u = 0.52 M_o = 41.2 \text{ ft-k}$

COL. STRIP WIDTH = $2 \times 14/4 = 7$ ft

FROM A.4 IN APPENDIX A, COL STRIP SUPPORTS:

75% INT. NEG. $M_u = 41.6 \text{ ft-k}$

75% EXT. NEG. $M_u = 15.5 \text{ ft-k}$

60% POS. $M_u = 24.7 \text{ ft-k}$

STRIP SPAN	COL STRIP	MIDDLE STRIP
INT. NEG.	41.6	13.9
EXT. NEG.	15.5	5.1
POS.	24.7	16.5



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LONG SPAN

$$M_o = \frac{(0.21A)(14)(16)^2}{8} = 95.9 \text{ ft-k}$$

FROM ACI 13.6.3

INT. NEG. $M_u = 67.1 \text{ ft-k}$

EXT. NEG. $M_u = 24.9 \text{ ft-k}$

POS. $M_u = 49.9 \text{ ft-k}$

FROM APPENDIX A.4

LONG SPAN	COL. STRIP	MIDDLE STRIP
INT. NEG.	50.3	16.8
EXT. NEG.	18.7	6.2
POS.	29.9	20

$$d^2 = \frac{M_u}{\phi \rho_t b (1 - 0.59 \rho_t f_y / f_c')} = \frac{M_u}{(0.9)(0.0206)(60,000)(12)(1 - (0.59)(0.0206)(60/4)}$$

$$d = \sqrt{\frac{M_u}{10,915}}$$

18ft SPAN: $d = \sqrt{\frac{16 \times 12}{33} \times \frac{12,000}{10,915}} = 2.53" \rightarrow \text{USE } 7"$

14ft SPAN: $d = \sqrt{\frac{12.83 \times 12}{36} \times \frac{12,000}{10,915}} = 2.2" \rightarrow \text{USE } 6"$

FOR SHRINKAGE & TEMP.

$$0.0018 \times 18" \times 12" = 0.173 \text{ in}^2$$

18ft SPAN: $f_{min} = \frac{0.173}{7 \times 12} = 0.0021$

14ft SPAN: $f_{min} = \frac{0.173}{6 \times 12} = 0.0024$



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	LOCATION	M _u (ft-k)	b (in)	d (in)	M _u x 12/b (ft-k)	ρ	A _s (in ²)	BARs
LONG SPAN								
1.	(2) HALF COL. INT. NEG.	50.5	84	7	7.2	0.0025	0.236	#5@12"
2.	EXT. NEG.	18.7	84	7	2.67	0.0021	0.2	#5@12"
3.	POS.	29.9	84	7	4.3	0.0021	0.2	#5@12"
4.	MIDDLE INT. NEG.	16.8	132	7	1.5	0.0021	0.2	#5@12"
5.	EXT. NEG.	6.2	132	7	0.6	0.0021	0.2	#5@12"
6.	POS.	20	132	7	1.8	0.0021	0.2	#5@12"
SHORT SPAN								
7.	EXT. COL. NEG.	15.5	42	6	4.4	0.0024	0.23	#5@12"
8.	POS.	24.7	42	6	7.1	0.0029	0.28	#5@12"
9.	MIDDLE NEG.	13.9	84	6	2.0	0.0024	0.23	#5@12"
10.	POS.	16.5	84	6	2.4	0.0024	0.23	#5@12"
11.	INT. COL. NEG.	41.6	42	6	11.9	0.005	0.48	#5@7 1/2"
12.	POS.	24.7	42	6	7.1	0.0029	0.28	#5@12"

$$M_u (12 \text{ in/ft}) = 0.9 A_s (\text{bars}) (d - \frac{1.96 A_s}{2})$$

1.	A _s = 0.236	→	0.236 / (8x12) = 0.0025 > 0.0021	OK
2.	A _s = 0.09	→	0.09 / (8x12) = 0.0009 < 0.0021	N.G.
3.	A _s = 0.14	→	0.14 / (8x12) = 0.0015 < 0.0021	N.G.
4.	A _s = 0.05	→	0.05 / (8x12) = 0.0005 < 0.0021	N.G.
5.	A _s = 0.019	→	0.019 / (8x12) = 0.0002 < 0.0021	N.G.
6.	A _s = 0.058	→	0.058 / (8x12) = 0.0006 < 0.0021	N.G.
7.	A _s = 0.17	→	0.17 / (8x12) = 0.0018 < 0.0024	N.G.
8.	A _s = 0.28	→	0.28 / (8x12) = 0.0029 > 0.0024	OK
9.	A _s = 0.075	→	0.075 / (8x12) = 0.0008 < 0.0024	N.G.
10.	A _s = 0.09	→	0.09 / (8x12) = 0.0009 < 0.0024	N.G.
11.	A _s = 0.48	→	0.48 / (8x12) = 0.0050 > 0.0024	OK
12.	A _s = 0.28	→	0.28 / (8x12) = 0.0029 > 0.0024	OK



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MEMO

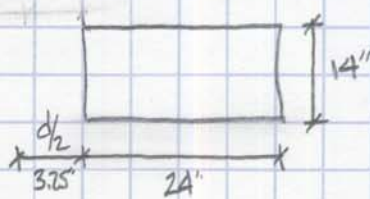
CONFERENCE

TELECON

ATTENDEES:

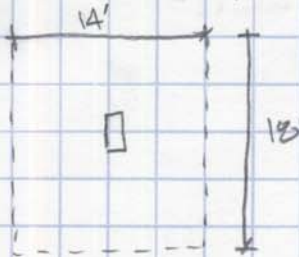
NOMINAL SHEAR STRENGTH

$$V_c = 4\sqrt{f'_c} b_o d \rightarrow \phi V_c = (0.75)(4)(\sqrt{4,000})(903)(6.5") = 111,366 \text{ lbs.}$$



BASED ON TRIBUTARY AREA

$$V_u = (214.2 \text{ psf})(18' \times 14') = 53,978 \text{ lbs.} < \phi V_c = 111,366 \text{ lbs.} \quad \text{OK}$$



∴ NO ADD'L SHEAR REINFORCEMENT REQUIRED

COL. DESIGN

$$P_n = 0.85f'_c A_c + A_s f_s \rightarrow \phi P_n = (0.65)(0.85)$$

$$\phi P_n = 0.65 [(0.85)(4,000)(336) + (4.00)(60,000)] = 898,560 \text{ lb}$$

$$a = \frac{A_s f_s}{0.85f'_c b} = 5.04$$

$$\phi P_n = 898,560 > P_u = 53,978 \text{ lbs.} \quad \text{OK}$$

$$M_n = 0.85f'_c ab \left(\frac{h}{2} - \frac{a}{2} \right) + A_s f_s \left(\frac{h}{2} - d' \right) + A_s f_s \left(d - \frac{h}{2} \right)$$

$$\phi M_n = 0.65 [(0.85)(4)(5.04)(14) \left(\frac{24}{2} - \frac{5.04}{2} \right) + (2)(60) \left(\frac{24}{2} - 2.5 \right) + (2)(60) \left(21.5 - \frac{24}{2} \right)]$$

$$\phi M_n = 247 \text{ ft-k} > M_o = 95.9 \text{ ft-k} \quad \text{OK}$$